

FOLLETT CORPORATION

12HI425A DISPENSER

DES. **J. ROBERSON**

JOB NO. **11-1420**

DATE **5/9/14**

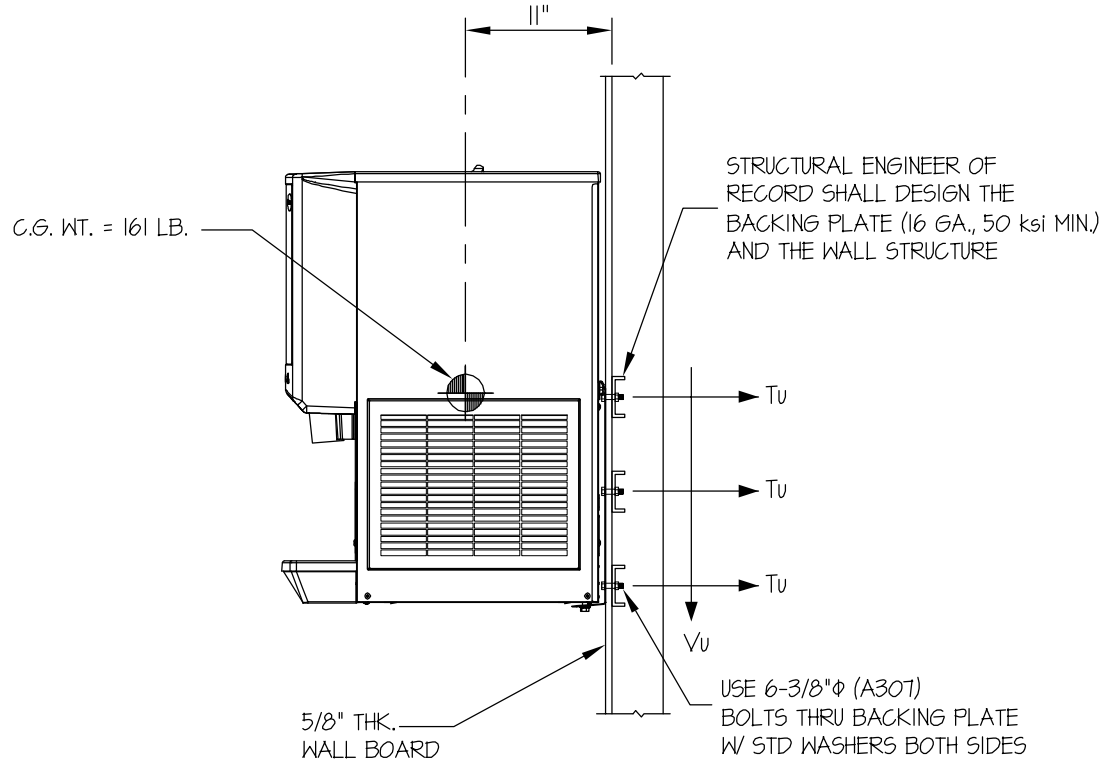
SHEET

1

OF **2** SHEETS

SEISMIC ANCHORAGE

WALL MOUNTED



$T_u = 421 \text{ LB/BOLT (MAX)}$
 $V_u = 157 \text{ LB/BOLT (MAX)}$

SIDE ELEVATION

NOTES:

- FORCES ARE DETERMINED PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10 STRENGTH DESIGN IS USED.

HORIZONTAL FORCE (E_h) = $1.80 W_p$ ($S_{ds} = 2.5, \alpha_p = 1.0, I_p = 1.5, R_p = 2.5, z/h \leq 1$)

VERTICAL FORCE (E_v) = $0.50 W_p$

- CENTER OF GRAVITY (C.G.) AND WEIGHT ARE THE GOVERNING PARAMETERS FOR DESIGN. THESE CALCULATIONS ENCOMPASS ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.
- STRUCTURAL ENGINEER OF RECORD FOR THE BUILDING SHALL PROVIDE SUPPORT STRUCTURE DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN IN COMBINATION WITH ALL OTHER LOADS THAT MAY BE PRESENT.



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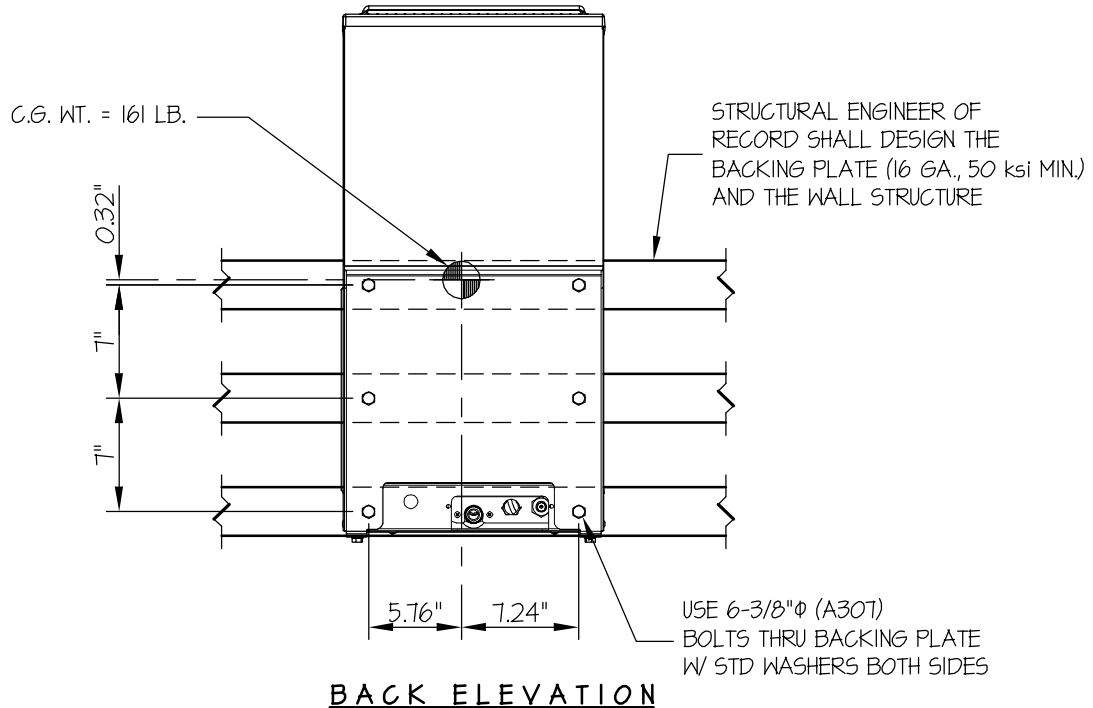
SHEET

2

OF **2** SHEETS

SEISMIC ANCHORAGE

WALL MOUNTED



BACK ELEVATION

LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

(STRENGTH DESIGN IS USED) ($S_{ds} = 2.5$, $a_p = 1.0$, $I_p = 15$, $R_p = 2.5$, $z/h \leq 1$)

WEIGHT = 161 LB

HORIZONTAL FORCE (E_h) = 1.80 $W_p = 290$ LB

VERTICAL FORCE (E_v) = 0.50 $W_p = 81$ LB

BOLT FORCES:

TENSION (T)

$$T_{U\text{ VERTICAL}} = \frac{(161\#)(1.2) + 81\#(11\')(7.24\')}{1\text{ BOLT}(14\')(13\')} = 120 \text{ LB/BOLT}$$

$$T_{U\text{ PARALLEL}} = \frac{290\#(11\')(14.32\')}{1\text{ BOLT}(13\')(14\')} = 251 \text{ LB/BOLT}$$

$$T_{U\text{ PERP.}} = \frac{290\#(14.32\')(7.24\')}{1\text{ BOLT}(14\')(13\')} = 166 \text{ LB/BOLT}$$

$$T_{U\text{ MAX}} = 120\# + (0.3)(166\#) + 251\# = 421 \text{ LB/BOLT (MAX)}$$

SHEAR (V)

$$V_{U\text{ MAX}} = \sqrt{\left(\frac{(161\#)(1.2\') + 81\#(7.24\')}{3\text{ BOLTS}(13\')}\right)^2 + \left(\frac{290\#(14.32\')}{2\text{ BOLTS}(14\')}\right)^2} = 157 \text{ LB/BOLT (MAX)}$$

BOLT SPEC: 3/8"φ (A307) BOLTS

φT = 3589 LB/BOLT

φV = 1914 LB/BOLT