

FOLLETT CORPORATION

DES. **J. ROBERSON**

SHEET

1

JOB NO. **11-1420**

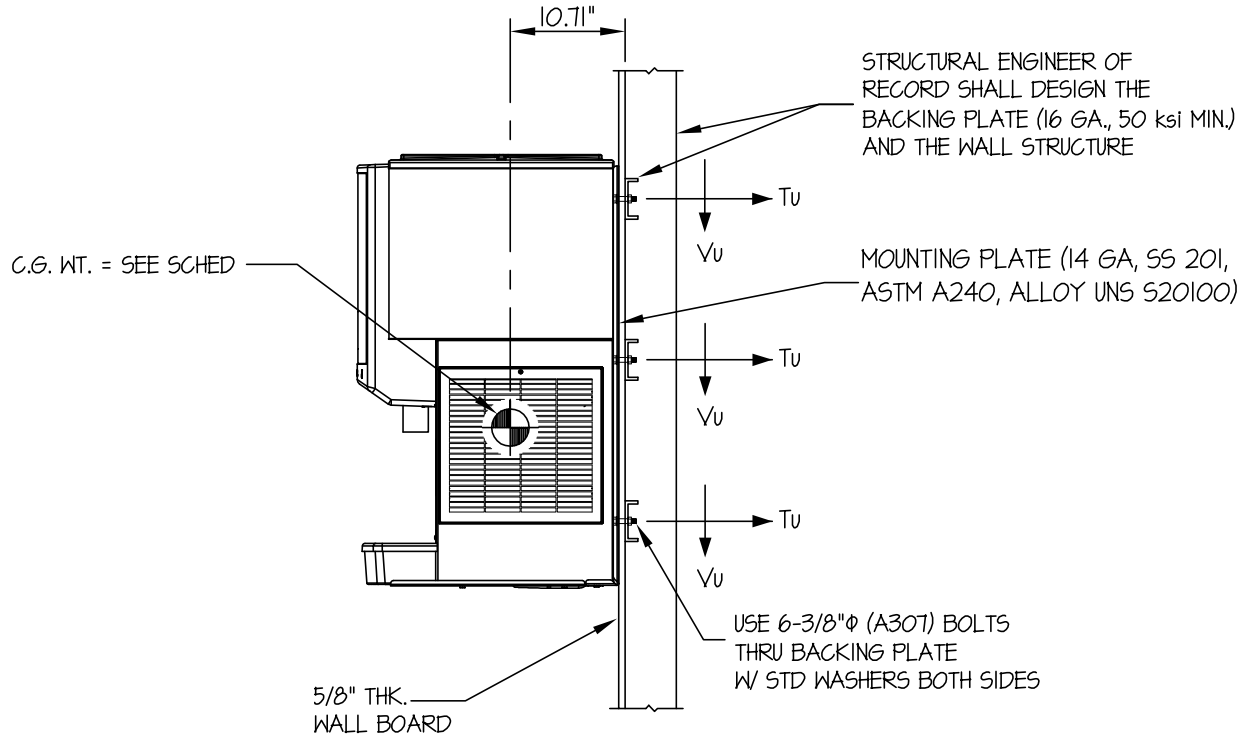
25/50 HI/HR 425 A/W DISPENSERS

DATE **5/22/14**

OF **2** SHEETS

SEISMIC ANCHORAGE

WALL MOUNTED



SIDE ELEVATION

NOTES:

- FORCES ARE DETERMINED PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10 STRENGTH DESIGN IS USED. ($S_{ds} = 2.5$, $a_p = 1.0$, $I_p = 1.5$, $R_p = 2.5$, $z/h \leq 1$)
HORIZONTAL FORCE (E_h) = 1.80
VERTICAL FORCE (E_v) = 0.50 W_p
- CENTER OF GRAVITY (C.G.) AND WEIGHT ARE THE GOVERNING PARAMETERS FOR DESIGN. THESE CALCULATIONS ENCOMPASS ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.
- STRUCTURAL ENGINEER OF RECORD FOR THE BUILDING SHALL PROVIDE SUPPORT STRUCTURE DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN IN COMBINATION WITH ALL OTHER LOADS THAT MAY BE PRESENT.



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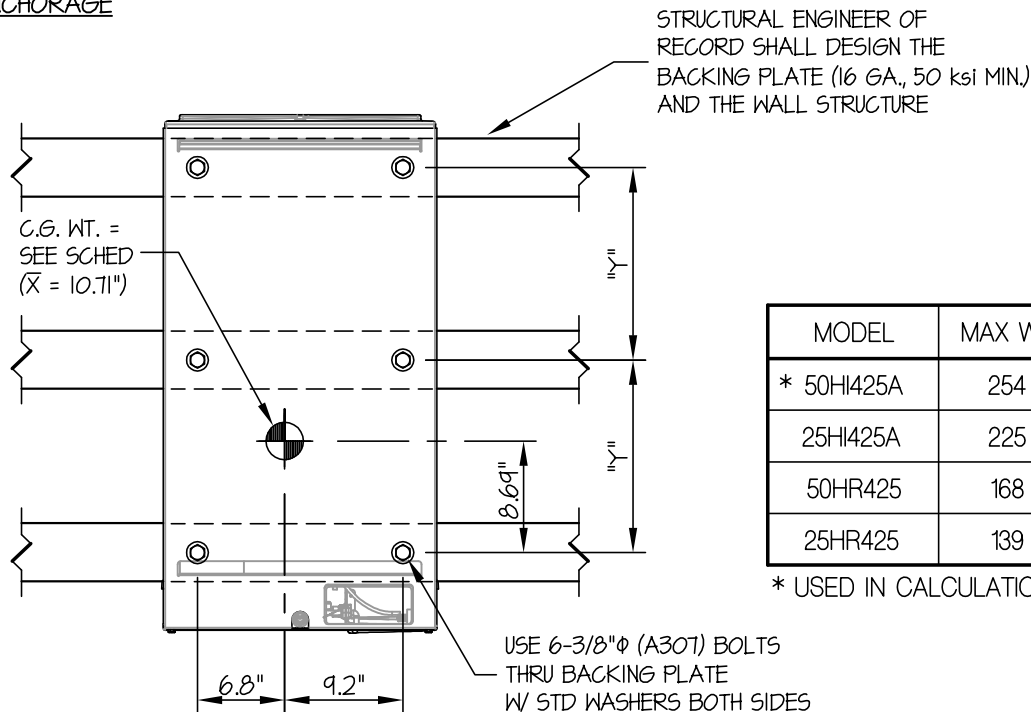
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WALL MOUNTED



MODEL	MAX WT	"Y"	T _u	V _u
* 50HI425A	254	15"	313	157
25HI425A	225	13"	319	154
50HR425	168	15"	208	104
25HR425	139	13"	198	96

* USED IN CALCULATION

BACK ELEVATION

LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

(STRENGTH DESIGN IS USED) ($S_{ds} = 2.5$, $a_p = 1.0$, $I_p = 1.5$, $R_p = 2.5$, $z/h \leq 1$)

WEIGHT = 254 LB

HORIZONTAL FORCE (E_h) = 180 W_p = 457 LB

VERTICAL FORCE (E_v) = 0.50 W_p = 127 LB

BOLT FORCES:

TENSION (T)

$$T_{u \text{ VERTICAL}} = \frac{(254\#)(1.2) + 127\#(10.71\#)(9.2\#)}{1 \text{ BOLT}(30\#)(16\#)} = 89 \text{ LB/BOLT}$$

$$T_{u \text{ PARALLEL}} = \frac{457\#(10.71\#)(8.69\#)}{1 \text{ BOLT}(16\#)(15\#)} = 178 \text{ LB/BOLT}$$

$$T_{u \text{ PERP.}} = \frac{457\#(8.69\#)(9.2\#)}{1 \text{ BOLT}(15\#)(16\#)} = 153 \text{ LB/BOLT}$$

$$T_{u \text{ MAX}} = 89\# + (0.3)(153\#) + 178\# = 313 \text{ LB/BOLT (MAX)}$$

SHEAR (V)

$$V_{u \text{ MAX}} = \sqrt{\left(\frac{(254\#)(1.2) + 127\#(9.2\#)}{3 \text{ BOLTS}(16\#)}\right)^2 + \left(\frac{457\#(8.69\#)}{2 \text{ BOLTS}(15\#)}\right)^2} = 157 \text{ LB/BOLT (MAX)}$$

BOLT SPEC: 3/8" (A307) BOLTS

$\phi T = 3589 \text{ LB/BOLT}$

$\phi V = 1914 \text{ LB/BOLT}$